AN INVESTIGATION OF THE BURN-IN AND RELATED PROBLEMS

by

Michael J. Lawrence

Operations Research Center

University of California, Berkeley

November 1964

ORC 64-32 (RR)

This research has been partially supported by the Office of Naval Research under Contract Nonr-3656(18) with the University of California. Reproduction in whole or in part is permitted for any purpose of the United States Government.

ABSTRACT

Two problems involving the derivation of bounds on distributions with a decreasing failure rate (DFR distributions) are presented.

Given that an item has a decreasing failure rate, sharp upper and
lower bounds on the burn-in time to achieve a specified mean residual life are derived. The bounds rely only on the DFR assumption and a knowledge of the first moment and a percentile of the
failure distribution.

An early estimate of the five year survival proportion (commonly called the five year cure rate) is of great interest in assessing
the value of a treatment for a mortal disease such as cancer. Assuming that the distribution of time to death is DFR and assuming
a knowledge of the mean and a percentile, sharp upper and lower
bounds on the survival proportion are obtained.

In addition some bounds on the hazard rate and density of a DFR distribution are given.

1. Introduction. The need for complex electronic equipment in locations where replacement of failed parts is impossible (e.g., ballistic missiles, satellites, etc.) has necessitated the production of very reliable components such as semiconductors. One method which is almost universally used to help achieve high reliability is to pre-age or burn-in the components to eliminate the "sports" or early failures. It has long been known that semiconductors, for example, exhibit infant mortality yet do not wear out (See: Blakemore, Kronson, Von Alven, 1963; Norris, 1963; Von Alven, 1962; and Von Alven, Blakemore, 1961); that is, they exhibit a decreasing failure rate (are DFR). The problem which now presents itself is how long to burn-in the component to achieve a specified reliability. The problem has been answered in the past by assuming a Weibull distribution of time to failure (Von Alven, 1962; Watson, Wells, 1961), for which there seems little statistical validation. However, this assumption is not necessary. It suffices to assume that the distribution is DFR and its first moment and a percentile are known in order to obtain sharp bounds on the residual mean life. It is a simple matter once the bounds are known to determine the minimum burn-in time to achieve a specified residual mean life. This is shown in section 2. Although the burn-in problem is developed in terms of a particular example, burning-in can clearly be used to advantage on any item which exhibits a decreasing failure rate.

A problem which bears some slight similarity to the burn-in problem is that of estimating the five year survival proportion in a

Berkson, Gage 1952. When a new treatment is tested clinically it is desirable to obtain an estimate, as early as possible, of its effectiveness. One objective indication of this is the five year survival proportion. Berkson and Gage (1952) have estimated a related quantity, the cure proportion, by assuming in the interests of mathematical expediency that the death rate due to cancer is a constant. It is well validated that the death rate from cancer is decreasing with time (Cutler, Axtell, 1963; Berkson, Gage, 1952) and this fact is used together with a knowledge of the mean and a percentile of the distribution of time to death, to obtain sharp upper and lower bounds on the five year survival proportion. This is discussed in section 3.

The most appealing feature of the solutions presented to the preceding two problems is that no assumption of a parametric expression for the probability distribution is made. Such an assumption would be very difficult to verify using the truncated data from semiconductor life tests or the small sample data resulting from a clinical trial. Yet it is possible to obtain a reasonable estimate of the mean life and early percentile for a truncated life test. This information together with the DFR assumption enables us to obtain bounds on the relevant quantities to be evaluated.

Nearly all the work completed to date on bounds for distributions possessing a monotone failure rate has been done by two authors, Barlow and Marshall (see: Barlow, 1963; Barlow and Marshall, 1963, 1964a and 1964b), who have often collaborated.

Barlow and Proschan (1964) also develop many applications of these bounds in the field of reliability theory.

Only the relevant bounds are set forth in sections 2 and 3, while the bounds are derived in section 4. A few additional theorems are added to complete the discussion of bounds for DFR distributions.

Mathematical Preliminaries. If the failure distribution F has density f, then the failure rate q(t) is defined for those values of t for which F(t) < 1 by

$$q(t) = \frac{f(t)}{\overline{F}(t)}$$

where $\overline{F}(t) = 1 - F(t)$ and it is assumed that $F(0^{-}) = 0$. The failure rate is also known as the hazard rate and by actuaries as the "force of mortality".

It can be readily verified that $q(t) = -\frac{d}{dt} \log F(t)$, when a density exists. Hence F is DFR (IFR) if $\log F(t)$ is convex on $[0,\infty]$ (concave where finite). This fact forms the basis of many of the proofs of section 4.

2. The Burn-in Problem. The only items which are burnt-in to any extent are semiconductors, although burn-in could well be applied more widely. Hence, we use semiconductors to illustrate our discussion of the burn-in problem.

A few remarks will made on the life distribution of a semiconductor since there is still some disagreement as to the actual shape of the distribution. Peck (Von Alven, 1962, Chapter 2) asserts that his data on semiconductors exhibits first an increasing failure rate and then a decreasing failure rate. He supports this by a physical explanation of the cause of the initial IFR. Other authors (i.e., Norris, 1963) maintain the distribution is DFR and the IFR, but this theory is more intuitive than well supported by life test data. The great bulk of work in the life testing of semiconductors supports the theory that there is no wear-out, and the failure rate is always decreasing. In particular, ARINC Research Corporation (Blakemore, Kronson, Von Alven, 1963; Von Alven, Blakemore, 1961) tested 10,300 individual devices with approximately 200,000 separate life test measurements and reported they could not detect any wear-out, but found in almost every case the life distribution was DFR.

The time to burn-in to achieve a specified reliability has been determined in practice by assuming the life distribution is either Weibull or lognormal. This affords a very rapid and simple method for evaluating the burn-in time but in the majority of cases where these distributions are assumed, it is done with little statistical validation.

A non-parametric approach based purely on the DFR assumption obviates this uncertainty of distribution validity and gives sharp bounds which although more conservative, does guarantee achieving the specified reliability since it is valid for a larger class of distributions.

Bounds are set out below on the survival probability and the residual mean life based on the assumption that the distribution is INTR and its mean and a percentile are known.

(2.1)
$$\frac{F \text{ DFR } \mu_1 = l \text{ , } F(\xi_p) = p \text{ and } \xi_p \le l \text{ or } l - p < e^{-\xi_p}}{e^{-b_l t}}, \quad 0 \le t \le \xi_p}$$

(2.2)
$$\overline{F}(t) \leq \frac{e^{-b_{\parallel}t}}{e^{-\alpha t}}, \quad 0 \leq t \leq \xi_{p}$$

where $\vec{F} = 1 - F$. The residual mean life at time t is denoted by μ_t

(2.3)
$$\mu_{t} = \frac{\int_{t}^{\infty} \overline{F}(x) dx}{\overline{F}(t)} \ge \int_{\overline{b}_{2}}^{(1 - \overline{b}_{1})} e^{b_{1}t} + \frac{1}{\overline{b}_{1}}, \quad t \le \xi_{p}$$

(2.4)
$$\mu_{t} = \frac{\int_{t}^{\infty} \tilde{F}(x) dx}{\tilde{F}(t)} \leq \frac{1}{\sigma} , \quad t \leq \xi_{p}.$$

Where α is the unique solution of

$$(2.5) \alpha e^{-\alpha \xi} p = 1 - p$$

and b₁, b₂ satisfy

Note that when distribution is DFR , $\xi_p \le l$ implies $l-p \le e^{-\xi}p$.

$$1 = \frac{1 - e^{-b_1} \xi_p}{b_1} + \frac{e^{-b_1} \xi_p}{b_2}$$

$$1 - p = e^{-b_1} \xi_p$$

The proofs of (2.1) through (2.4) are given in theorems (4.2) through (4.5) of Section 4.

The most interesting result, the lower bound on the mean residual life, is useful only up to time ξ_p , for after this time the bound is constant and so gives no indication of the effect of increased burn-in. However, even in the light of this, the restriction on the percentile that $\xi_p \leq 1$ or $1-p \leq e^{-\xi_p}$ does not appear restrictive in the burn-in problem as it is unlikely that the item would be burnt-in for a time greater than its mean life.

By the use of equation (2.3), the burn-in time to achieve a specified mean residual life has been calculated and is given in tables 1 through 3.

Bounds in terms of the first and second moment have little usefulness since the sharp lower bound on the mean residual life in this case is the value of the mean, thus giving no indication of the benefit gained by burn-in. Bounds on the survival probability for this case have been calculated by Barlow and Marshall (1963).

The burn-in of semiconductors is sometimes carried out at an increased stress to accelerate the ageing, (see Norris, 1963). This may introduce many complications in the prediction of the optimal burn-in time. However, it will be assumed that it is possible to convert from the un-accelerated burn-in time to the accelerated burn-in

time. This could possibly be done with the use of the Arrhenius relation, although Yon Alven states that the Eyring relationship may possibly be better.

Personal communication.

TAPLE 1

LUMER BUUND EN PLAN-IN TIME TO ACHIEVE RESIDUAL MEAN LIFE = 1.25

47 0		5 · 3	•	•		J.) • ()	5
10.0	٠ ر ر د	7 .0.	£ () 3	530.	.001	()	())
2.02	~	150700		J + 33 • 1	C. C. 3.P	おくししょう	0.000.0
1.03	376.	13	.010	.cc1	٠()٠	• CC4	, CC?
7.)4	.027	.618	.913	.010	1000	37J.	575.
	.035	.623	.(17	.012	500.	127.	. ((4
	.044	.029	073	.015	. (11	822.	.006
10.0	.053	.134	.024	.C18	.013	.01C	.001
0	.062	.C4C	.028	.021	.015	.011	· CCE
	10.	• 646	.632	.024	0•	• 1	500.
0.10	:.0c36	, n	. C 3.7	.02	.020	٠٠] ۶	ر ۱۷
1.20		7	.094	.060	.043	Tiù.	(21
J. 30		•	1.51.	L.1C35	C.0716	6640.0	5260.0
0.40			. 268	.160	.105	11.3.	347
J.50	- .		.461	.233	.147	957.	260
7.60				.356	.201	.125	(75
0.10				.551	.272	159	550
J.8C					.376	-2CC	112
06.0					.514	152.	734
0					. 152	.315	15€
- c	entr in	the table ind	licates the	Sur is ti	ше ехсеела	ئ ئ	

TAHLE 2

1.50		I	ζ	~	_	_ت	80	9	2	4	٣	~	2	7	7	\$	•	9	2	ပ
н	5.	C	ر	0.0	C	CC	ر 1	1	(1)	C.		7	5	(1)		C 1	4.1	.157	C .	~
LIFE	U	j	ن	ن	ر،	ပ	ပံ	ٺ	ن	ن	ن	ن	ن	ن	ن	ز	ز	ئ	J	ပ
VEAN	د • د	.002	٠(,).	.0.7	31C.	-012	.015	.Cle	.021	\circ	٠٠٧	.056	.689	.126	.169	.218	.275	C.3431	474.	.523
VE RESIDUAL	6.1	.003	.006	.010	.013	.017	.621	.024	.C2H	~	.33	.C78	.121	.185	.756	. 344	155.	6.6662	.816	
TC ASPIR	4 •	ان ان	£30.	.113	.C18	. C 2 3	9	.033	.C 3R	.543	. (48	101	.142	.277	0.40.20	. 586				
PA-IN IINT	C . S		٠٠ 1 ك	• () e	77.	• • •		• 5 44	157.	5	• î 6 6	5 [. 13.					į		
NF CN PLE	•	a: →	310	570	770	243	S	0.62	210	a,	0.0346									
BCL	- /	. ,				- 1				- **			-	le:	·			_		
LUWER	4	0.01	1.72	£ 0.0	40.6	3.05	90.6	2000	7.08	90.0	J.13	J.20	J. 30	04.0	0.50	1.4.1	7.10	റ∙ 8≎	J. 90	1.30

o erer, in the raple in tipares the lumb-in time exceeds :-. u.

TABLE 3

LOWER BOUND ON PURN-IN TIME TO ACHIEVE RESIDUAL MEAN LIFE = 2.CC

8:	C C 3	900	600	C12	C.C153	C 18	021	C 24	027	.031	. C 64	C.0597	121.	.178	.222	.27C	. 322	.379	.442
⊙. 8 ⊙	400°	.00B	.013	.617	C.022C	.026	.031	.035	.040	.045	*60	C-1494	.210	.278	.355	.443	.544	.662	.802
0.70		.011	.017	.023	C.0297	.035	.042	.048	.054	.061	.130	C.211C	. 364	+14.	.546				
9.0	• 000	.013	.020	. 627	0.0342	.041	.048	.055	.063	.070	.153	0.2502	.366						
9:0	.003	• (15	. (23	.631	9563.0	. 547	. C 56	.664	.073	.082	0.1798	. 298							
0.55	.0 c	.017	.026	.036	0.0455	.055	.064	.074	.085	0.0955	:						1		
	0	0	0	0.	0.05	0	0	•	0	. 1	0.20	0.30	•	•	•	•	ე 80 • ი	•	1.00

No entry in the table indicates the burn-in time exceeds N. B.

3. Bounding the Survival Proportion. A frequently used objective index of the effectiveness of a treatment is the proportion of patients surviving the disease for five years. (See for example, Berkson, Gage, 1952). This will be called the five year survival proportion although it has been generally called by the misleading name of "five year cure rate" by the medical profession. Clearly the word cure is inappropriate as even in so mortal a disease as cancer it is not certain that the patient is cured when he has survived five years.

Berkson and Gage (1952), have discarded the idea of a survival percentage in favour of computing the cure proportion; defining the patient cured when his death rate is the same as the normal mortality rate. Cutler and Axtell (1963) point out that in some cancers this is never achieved and they redefine cure as the achievement of a stabilized death rate. But with both Berkson, et al and Cutler, et al, information is required over a long span of time to estimate the cure proportion.

Although the five year survival proportion does not give as accurate a picture as the cure proportion (where the latter is relevant) it does afford a good indication of the effectiveness of a treatment and can be calculated more simply and at an earlier time than can the cure proportion.

An extension of the work already done in this field would be to predict the five year survival proportion at the end of only say one year of a clinical trial, thus enabling an early assessment of the treatment to be made.

The mathematical model will be simplified by assuming that the probability of death due to normal causes is independent of the probability of death due to cancer. This clearly oversimplifies the issue but Berkson and Gage (1952) maintain that this assumption does give reasonable results. Thus

(3.1)
$$\mathbf{F}(t) = \mathbf{F}_{\mathbf{r}}(t) \mathbf{F}_{\mathbf{r}}(t)$$

where F(t) is the survival probability in time t and $F_n(t)$ and $F_c(t)$ are respectively the probabilities of death from "normal causes" and from cancer in time t. It is assumed that F_n is known from life tables. Also

(3.2)
$$q(t) = q_c(t) + q_n(t)$$

where q(t) is the death rate at time t and the subscripts c and n are as in (3.1).

Berkson and Gage (1952) have shown that $q_c(t)$ is decreasing at a rate which is a function of the mean time to death of the untreated patients. The normal mortality rate, $q_n(t)$, is increasing. Thus q(t) is initially decreasing and then increasing.

If the time at which q(t) changes from decreasing to increasing is large compared with 5 years, bounds on F_c (5 years) may be estimated by assuming that F is DFR. Thus from a knowledge of the mean and a percentile of F, bounds on F (5 years) may be determined by using equations (2.1) and (2.2), and from this F_c (5 years) can easily be determined from equation (3.1).

A less accurate but surer method would be to adjust the observations of the time to death to obtain an estimate of the DFR distribution F_c . Hence by a straightforward application of the DFR bounds, we may obtain bounds on F_c (5 years).

Bounds on the failure rate at five years may also be evaluated to give a further indication of the effectiveness of the treatment.

These bounds can be estimated by the use of the DFR bounds given below and equation (3.2)

F DFR,
$$\mu_1 = 1$$
, $F(\xi_p) = p$ and $\xi_p \le 1$ or $1 - p < e^{-\xi}p$

$$(3.3) q(t^+) \geq \alpha$$

where α is defined by the unique solution to (2.5).

(3.4)
$$q(t^{-}) \leq \begin{cases} \infty & t = 0 \\ b_{1} & t > 0 \end{cases}$$

See theorems (4.6) and (4.7) for proofs.

4. Bounds on DFR Distributions.

4.1. Bounds Given the Mean and a Percentile have great appeal since good estimates of these two quantities can be obtained from limited life test data. In addition, the desired bounds are all nontrivial which is in contrast to the case where the first two moments μ_1 and μ_2 are given. In this case the lower bound on the mean residual life is trivial and sharp (i.e. is the value μ_1).

The DFR distribution with mean $\mu_1 = 1$ implies an upper bound on the percentile. The lower bound is zero, and both bounds are sharp.

(4.1)
$$0 \le 1 - p \le \begin{cases} e^{-\xi}p, & \xi_p \le 1 \\ (\xi_p e)^{-1}, & \xi_p > 1 \end{cases}$$

This result is proved by Barlow and Marshall (1963).

Two distributions will be defined. Let

(4.2)
$$\overline{J}_{b_1}(x) = \begin{cases} \beta e^{-b_1 x} & , & x \leq \xi_p \\ (1-p) e^{-(x-\xi_p)b_2} & , & x > \xi_p \end{cases}$$

where
$$\overline{J}_{b_1} = 1 - J_{b_1}$$
,

and β and b_2 are given by

(4.3)
$$\beta e^{-b_1 \xi} P = 1 - p$$
, $(0 < \beta < 1)$

and
$$\int_0^\infty \overline{J}_{b_1}(x) dx = 1 ;$$

Clearly J_{b_1} has mean $\mu_1 = 1$ and p^{th} percentile ξ_p .

Let K_{b_1} be the subclass of J_{b_1} which is DFR . A

lemma will now be proved to facilitate the proof of theorem 4.1.

Lemma 4.1. If the p^{th} percentile ξ_p of K_{b_1} satisfies the conditions (4.1) then the distribution of the class K_{b_1} which gives the maximum value to the mass at the origin is $K_{b_1}^*$, where b_1^* is the minimum value of b_1 such that $b_1 = b_2$; i.e., an exponential on $[0,\infty]$, with possible mass at the origin.

<u>Proof.</u> Clearly the distribution of the class J_{b_1} which attains maximum mass at the origin is given by $b_1 = 0$; but it is not DFR since it must be log concave. As b_1 increases from zero (thus decreasing β), b_2 increases but less rapidly, and the distribution will first be DFR when $b_1 = b_2$, attaining then the maximum mass at the origin for a distribution R_{b_1} . The equation of this distribution is

(4.4)
$$K_{b_1 = b_2}(x) = \alpha e^{-\alpha x}$$

where α is the minimum solution of

$$(4.5) 1 - p = \alpha e^{-\alpha \xi} p$$

$$\alpha \le 1$$

Note that a solution α is guaranteed by the conditions on the percentile, and that for $\xi_p \leq 1$ the solution to (4.5) is unique, but for $\xi_p \geq 1$ there may be two solutions.

Theorem 4.1. If F is DFR with mean $\mu_l=1$, and p^{th} percentile ξ_p is given and satisfies the condition $1-p < e^{-\xi_p}$, then

$$F(x) \ge \alpha e^{-\alpha x}$$
, $x \le \xi_p$
 $F(x) \le \alpha e^{-\alpha x}$, $x \ge \xi_p$

and α is defined as the unique solution of $\alpha e^{-\alpha \xi} P = 1 - p$.

Proof. Suppose that the theorem is false. Then by convexity, either (i) or (ii) is true.

(i)
$$\overline{F}(x) \le \alpha e^{-\alpha x}$$
, for some $x \le \xi_p$

(i)
$$\overline{F}(x) \le \alpha e^{-\alpha x}$$
, for some $x \le \xi_p$
(ii) $\overline{F}(x) \ge \alpha e^{-\alpha x}$, for some $x \ge \xi_p$ and $\overline{F}(x) \ge \alpha e^{-\alpha x}$
for $x \le \xi_p$.

Suppose case (i):

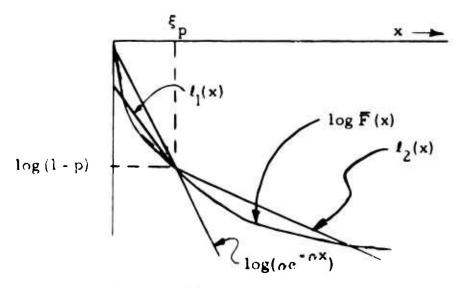


Figure 4.1

By log convexity $\overline{F}(x) > \alpha e^{-\alpha x}$ when $x > \xi_p$. Construct two exponential curves, $e^{-l_1(x)}$ and $e^{-l_2(x)}$ where $l_1(x)$ and $\ell_2(x)$ are linear in x and such that

$$e^{-\boldsymbol{\ell}_{1}(\xi_{p})} = e^{-\boldsymbol{\ell}_{2}(\xi_{p})} = 1 - p$$

$$\int_{0}^{\xi_{p}} \left\{ \overline{F}(x) - e^{-\boldsymbol{\ell}_{1}(x)} \right\} dx = 0$$

$$\int_{\xi_{p}}^{\infty} \left\{ F(x) - e^{-\boldsymbol{\ell}_{2}(x)} \right\} dx = 0 .$$

Now clearly $e^{-\ell_2(x)} > \alpha e^{-\alpha x}$ for $x > \xi_p$ and hence $e^{-\ell_1(x)} < \alpha e^{-\alpha x}$ for $x < \xi_p$. Thus a DFR distribution has been constructed with the same mean and percentile as the exponential $\overline{K}(x) = \alpha e^{-\alpha x}$, but a greater mass at the origin, which by lemma 4.1 is impossible.

Suppose case (ii):

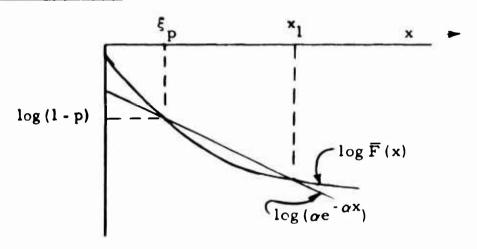


Figure 4.2

By log convexity of DFR distributions there must be a single crossing, say at x_1 , where $x_1 > \xi_p$. By assuming a percentile at x_1 , and noting that the solution α is unique since $1 - p < e^{-\xi}p$, it can be seen from case (i) that case (ii) is impossible.

Note that the condition on the percentile $-1-p < e^{-\frac{\xi}{p}}P$ which it was necessary to assume to assure a unique value of $-\sigma$ is always satisfied by a DFR distribution for $-\xi_p \le 1$.

It does not appear likely that this restriction will limit the applicability of the bounds as it is hard to imagine estimating a percentile at $\xi_p > 1$ in a distribution. In order to prove some theorems on bounds, a class of DFR distributions \overline{G}_T is posited with mean $\mu_1 = 1$ and p^{th} percentile ξ_p satisfying $1 - p < e^{-\xi} p$.

$$\frac{T < \xi_{p}}{\overline{G}_{T}(x)} = \begin{cases} e^{-b_{1}x} & , & 0 \le x \le T \\ e^{-b_{2}x + (b_{2} - b_{1})T} & , & x > T \end{cases}$$

where b₁ and b₂ satisfy

(4.7)
$$1 = \frac{1 - e^{-b_1 T}}{b_1} + \frac{e^{-b_1 T}}{b_2}$$

(4.8)
$$1 - p = \exp(-b_2 \xi_p + (b_2 - b_1) T)$$

and for this class to be DFR, $b_2 \le b_1$.

$$\frac{T \ge \xi_{p}}{\overline{G}_{T}(x)} = \begin{cases} e^{-b_{1}x} & , & 0 \le x \le T \\ e^{-b_{2}x + (b_{2} - b_{1})T} & , & x > T \end{cases}$$

 b_1 and b_2 satisfy (4.7) and

$$(4.10) 1 - p = e^{-b_1 \xi} p$$

and b < b for G_T to be DFR.

Lemma 4 2 Assuming $1-p \le e^{-\xi}P$ for every $T < \xi_p$ there is a solution of (4.7) and (4.8) continuous in T, and for every $T \ge \xi_p$ there is a solution of (4.7) and (4.10) continuous in T.

<u>Proof:</u> $T \le \xi_p$: By substituting for b_2 from (4.7) into (4.8) we

obtain

$$1 - p = \exp \left\{ -b_1 T - e^{-b_1 T} (\xi_p - T) (1 + \frac{e^{-b_1 T} - 1}{b_1})^{-1} \right\}$$

and it is desired to show this always has a solution $\ b_1$. Since the distribution is IFR and $1-p\le e^{-\xi}p$, we see $\ b_1\ge 1$.

Let

Now

$$h(b_1) = \exp\left\{-b_1 T - e^{-b_1 T} (\xi_p - T) (1 + \frac{e^{-b_1 T} - 1}{b_1})^{-1}\right\} - 1 + p$$

$$\lim_{b_1 \to 1} h(b_1) = e^{-\xi} p - 1 + p \ge 0$$

 $\lim_{b_1 \to \infty} h(b_1) = -1 + p < 0$

Thus as the function is clearly continuous in b_1 , there exists a solution such that $h(b_1) = 0$.

Since $b_1 \ge 1$ and the mean $\mu_1 = 1$, \overline{G}_T must cross e^{-x} once from below and thus $b_2 \le b_1$.

 $T > \xi$: From (4.10) it can be seen that there is always a solution for b_1 .

i.e.
$$b_1 = -\frac{1}{\xi_p} \log (1-p)$$
.

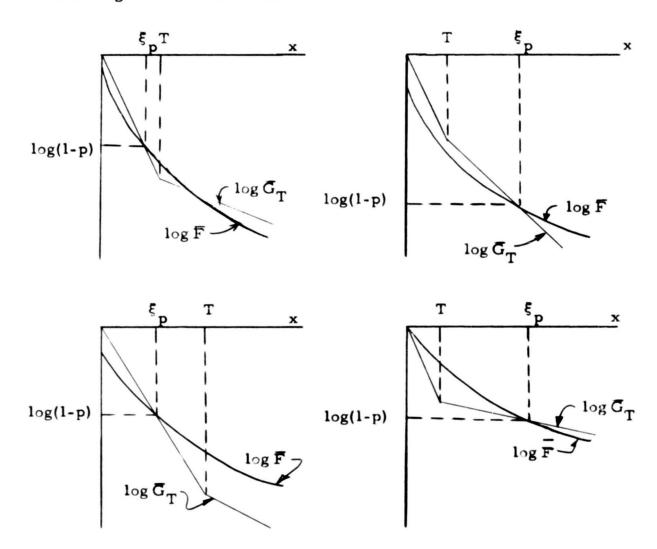
Hence
$$b_2 = \exp\left(\frac{T}{\xi_p}\log(1-p)\right)\left\{1 + \frac{1 - \exp\left(\frac{T}{\xi_p}\log(1-p)\right)}{\xi_p^{-1}\log(1-p)}\right\}^{-1}$$

which has a solution continuous in T for all $T > \xi_{D}$.

Since $1-p \leq e^{-\xi} p$ and $\mu_1=1$ it can clearly be seen that $b_2 \leq b_1$. $\|$

Note that $\lim_{T\to 0} \overline{G}_T(x) = \alpha e^{-\alpha x}$ where α is defined uniquely by (4.5). This limit will be denoted by $\overline{G}_0(x)$.

Use is made in the following theorems of the fact that G_T and F must cross at least once if they have the same first moment. The various possibilities for the intertwining of $\log \overline{G}_T$ and $\log \overline{F}$ are shown below.



Theorem 4.2: If F is DFR and has first moment $\mu_1 = 1$ and p^{th} percentile ξ_p given, and also $1 - p < e^{-\xi}p$, then

$$\overline{F}(t) \leq \begin{cases} e^{-b_1 t} & , & 0 \leq t \leq \xi_p \\ \alpha e^{-\alpha t} & , & t > \xi_p \end{cases}$$

and the inequalities are sharp. b_1 is defined by equation (4.10) and α by equation (4.5).

Proof:

$$\frac{0 \le t \le \xi_{p}}{\overline{F}(t) \le \overline{G}_{\xi_{p}}(t)}, \quad 0 \le t \le \xi_{p}$$

$$\frac{t \ge \xi_{p}}{\overline{F}(t) \le \overline{G}_{0}(t)}, \quad t \ge \xi_{p}.$$

Theorem 4.3: If F is DFR and has $\mu_l = 1$ and p^{th} percentile ξ_p given and also $1 - p < e^{-\xi}p$; then

$$\overline{F}(t) \ge \begin{cases} \sigma e^{-\sigma t} & , & 0 \le t \le \xi_p \\ e^{-b_l t} & , & t > \xi_p \end{cases}$$

where b_1 is defined by (4.10) and α by (4.5). The bound is sharp.

Proof:

 $0 \le t \le \xi_p$: This bound follows directly from theorem 4.1.

 $\frac{\xi_p < t \le \infty}{-}$: The proof is obvious. The bound is "epsilon"

attained by $\lim_{T \to \infty} \overline{G}_T(x)$.

Theorem 4.4: If F is DFR, $\mu_l = l$ and the p^{th} percentile ξ_p given and also $1-p < e^{-\xi}P$; then

$$\frac{\int_{t}^{\infty} \overline{F}(x) dx}{\overline{F}(t)} \geq \begin{cases} \frac{(1-\frac{1}{b_{1}}) e^{b_{1}t} + \frac{1}{b_{1}}}{\frac{1}{b_{2}}}, & t \leq \xi_{p} \\ \frac{1}{b_{2}}, & t \geq \xi_{p} \end{cases}$$

where b_1 is defined by equation (4.10) and b_2 is defined by the equations (4.7) and (4.10) with $T = \xi_p$.

Proof:

For
$$t \leq \xi_p$$
: Since $\overline{F}(x) \leq \overline{G}_{\xi_p}(x)$, $x \leq \xi_p$

$$\int_t^{\infty} \overline{F}(x) dx \geq \int_t^{\infty} \overline{G}_{\xi_p}(x) dx$$
, $t \leq \xi_p$

therefore

$$\frac{\int_{t}^{\infty} \overline{F}(x) dx}{\overline{F}(t)} \geq \frac{\int_{t}^{\infty} \overline{G}_{\xi_{p}}(x) dx}{\overline{G}_{\xi_{p}}(t)} = (1 - \frac{1}{b_{1}}) e^{b_{1}t} + \frac{1}{b_{1}}$$

 $\frac{For\ t>\xi_p}{p}:\ The\ proof\ will\ be\ treated\ in\ two\ cases\ based}$ on the crossings of $\overline{G}_{\xi_p}(x)\quad and\quad \overline{F}(x)\quad for\quad x\geq\xi_p\ .$

Case (i): Consider the extremal distribution $G_{\xi_p}(x)$ and let it cross F(x) at $u(\xi_p) \ge \xi_p$. Obviously due to log convexity the crossing is from above.

Since
$$\overline{F}(x) \leq \overline{G}_{\xi}(x)$$
 $x \leq u(\xi_p)$

$$\frac{\int_{t}^{\infty} \overline{F}(x) dx}{\overline{F}(t)} \geq \frac{\int_{t}^{\infty} \overline{G}_{\xi}(x) dx}{\overline{G}_{\xi}(t)} \qquad t \leq u(\xi_p)$$

Now by Theorem 4.1 $\overline{F}(x) \leq \overline{G}_0(x)$ for $x \geq \xi_p$. Thus due to log convexity of $\overline{F}(x)$, for every x, $u(\xi_p) \leq x \leq \infty$, it is always possible to find a value T, $0 \leq T \leq \xi_p$, such that u(T) = x.

$$\frac{\int_{t}^{\infty} \overline{F}(x) dx}{\overline{F}(t)} \geq \inf_{T \leq \xi_{p}} \frac{\int_{t}^{\infty} \overline{G}_{T}(x) dx}{\overline{G}_{T}(t)} \qquad t \geq u(\xi_{p})$$

Case (ii): $u(\xi_p) = \xi_p$. By a similar reasoning to case (i) it may be shown

$$\frac{\int_{t}^{\infty} \overline{F}(x) dx}{F(t)} \geq \inf_{T \leq \xi_{p}} \frac{\int_{t}^{\infty} \overline{G}_{T}(x) dx}{\overline{G}_{T}(t)}, \quad t \geq \xi_{p}$$

$$= \inf_{T \leq \xi_{p}} \frac{1}{b_{2}}$$

$$= \frac{1}{b_{2}} \text{ where } b_{2}^{*} \text{ is the value of } b_{2}$$

calculated at $T = \xi_{p}$.

Thus, the lower bound for the mean residual life while not trivial for $t \geq \xi_p$ is nevertheless not dependent on t and so can give no information on the merit of continued burn-in.

Theorem 4.5: If F is DFR and $\mu_l = l$ and the p^{th} percentile ξ_p is given and also $l-p < e^{-\xi}P$; then

$$\frac{\int_{t}^{\infty} \overline{F}(x) dx}{F(t)} \leq \frac{\int_{t}^{\infty} \overline{G}_{0}(x) dx}{\overline{G}_{0}(t)} = \frac{1}{\alpha}, \quad t \leq \xi_{p}$$

Proof: The proof follows directly from theorem 4.3.

Theorem 4.6: If F is DFR with first moment $\mu_1=1$ and p^{th} percentile ξ_p , and $1-p \le e^{-\xi}P$, and has hazard rate q then , $q(t^+) \ge \alpha$, where α is the solution of (4.5).

The bound is sharp.

Proof: The proof follows directly from Theorem 4.1.

Theorem 4.7: If F is DFR with $\mu_l = l$ and p^{th} percentile ξ_p and $l-p \le e^{-\xi}P$ and hazard rate q then

$$q(t^{-}) \leq \begin{cases} \infty & , & t = 0 \\ b_1 & , & t > 0 \end{cases}$$

where b_1 is the solution of (4.7) and (4.8) for T=t, $t<\xi_p$; and b_1 is the solution of (4.10) for $t\geq\xi_p$. The bound is sharp.

Proof: t = 0 The bound is trivial and is attained by the distribution \overline{G}_{C} .

 $0 < t \le \xi_p$: By the log convexity of the DFR distribution it can be seen that at t

$$q(t) \leq b_1$$

 $t \geq \xi_p$ Clearly by log convexity

$$q(t^{-}) \leq b_{1} .$$

The bound is relatively trivial and is "epsilon attained" by the distribution $\lim_{T\to\infty} \overline{G}_T \cdot \|$

4.2. Bounds Assuming the First Two Moments Are Given.

Barlow and Marshall (1964) have given bounds on the survival probability of the DFR distribution when the first two moments are given. The same methods used to bound the survival probability may be used to obtain sharp bounds on the residual mean life, the failure rate and the density of the distribution. These bounds are stated below and proofs for them may be found in Lawrence (1964).

(4.11)
$$\mu_{t} = \frac{\int_{t}^{\infty} \overline{F}(x) dx}{\overline{F}(t)} \geq \mu_{1}$$

(4.12)
$$\mu_{t} = \frac{\int_{t}^{\sigma} \overline{F}(x) dx}{\overline{F}(t)} \leq \frac{1}{a_{t}^{2}}$$

$$(4.13) q(t^{-}) \leq a_{1}^{*}$$

$$(4.14) q(t^{+}) \geq a_{2}^{*}$$

•

$$(4.16) f(t^{+}) \geq \begin{cases} \inf & \sigma^{2} \exp(-\sigma t) \\ \frac{2}{\mu_{2}} \leq \sigma \leq 1 \\ \inf & a_{2} \exp\{-a_{2}t + (a_{2} - a_{1})T\} \end{cases}, \quad 0 \leq t \leq \frac{\mu_{2}}{2} \\ \inf & a_{2} \exp\{-a_{2}t + (a_{2} - a_{1})T\} \end{cases}, \quad t \geq \frac{\mu_{2}}{2}$$

Where a_1^* , a_2^* are the unique solutions of (4.17) and (4.18) with

$$(4.17) 1 = a_1^{-1} (1 - \exp(-a_1 T)) + a_2^{-1} \exp(-a_1 T)$$

(4.18)
$$\frac{\mu_2}{2} = a_1^{-2} \{1 - (a_1 T + 1) \exp(-a_1 T)\} + a_2^{-2} (a_2 T + 1) \exp(-a_1 T)$$

REFERENCES

- Barlow, R. E., (1963), Bounds on Integrals with Application to Reliability Problems, Operations Research Center 63-27 (RR), University of California, Berkeley, California (to appear in Ann. Math Stat.)
- Barlow, R.E., and A. Marshall, (1963), Tables of Bounds for Distributions with Monotone Hazard Rates. Boeing Scientific Research Laboratories, Math. D1-82-0249
 - Rate I and II, "Ann Math Stat., Vol. 35, No. 3, pp. 1234-1274.
- Research Center 64.9 (RR), University of California, Berkeley, California
- Barlow, R.E., and F. Proschan, (1964), Mathematical Theory of Reliability, John Wiley and Sons, New York
- Berkson, J., and R. P. Gage, (1952), "Survival Curve for Cancer Patients Following Treatment," J. Amer. Stat. Assoc., Vol. 47, No. 259, pp. 501-515.
- Blakemore, G. J., E. T. Kronson, and W. H. Von Alven, (1963), Semiconductor Reliability, ARINC Research Corp. Publication No. 339-01-4-303
- Cutler, S. J., and L. M. Axtell, (1963, "Partitioning of a Patient Population with Respect to Different Mortality Risks," J. Amer. Stat. Assoc, Vol. 58, No. 303, pp. 701-712.
- Grenander, V., (1956), "On the Theory of Mortality Measurement Part II," Skand. Akt Tidskrift, Vol. 39, No. 3-4, pp. 126-153
- Hausman, W.H. and M. Kamins, (1964), Early Failures in Automobile Parts: A Background Study in Reliability, RAND Corporation, Memorandum RM-4002-PR
- Lawrence, M. J. (1964). "An Investigation of the Burn-In and Related Problems," Masters Thesis, Operations Research, University of California, Berkeley, California
- Norris, R.H., (1963), "Run-In or Burn-In of Electronic Parts,"

 Proceedings, Ninth National Symposium on Reliability and
 Quality Control, pp. 335-357

- Von Alven, W.H., (1962), Semiconductor Reliability, Vol. 2, Engineering Publishers.
- Von Alven, W.H., and G.J. Blakemore, (1961), Reliability of Semiconductor Devices, Final Report ARINC Research Corp. Publication No. 144-6-270.
- Watson, G.S., and W.T. Wells, (1961), "On the Possibility of Improving the Mean Useful Life of Items by Eliminating Those with Short Lives, <u>Technometrics</u>, Vol. 3, No. 2, pp. 281-298.

BASIC DISTRIBUTION LIST FOR UNCLASSIFIED

TECHNICAL REPORTS

Logistics and Mathematical Statisites Branch Office of Naval Research Washington, D.C. 20360

Commanding Officer
Office of Naval Research Branch
Office
Navy No. 100 Fleet Post Office
New York, New York

Defense Documentation Center Cameron Station Alexandria, Virginia 22314

Defense Logistics Studies Information Exchange Army Logistics Management Center Fort Lee, Virginia Attn: William B. Whichard

Technical Information Officer Naval Research Laboratory Washington, D.C. 20390

Commanding Officer
Office of Naval Research Branch
Office
207 West 24th Street
New York, New York 10011
Attn: J. Laderman

Commanding Officer
Office of Naval Research Branch
Office
1030 East Green Street
Pasadena, California 91101
Attn: Dr. A.R. Laufer

Bureau of Supplies and Accounts Code OW Department of the Navy Washington, D.C. 20360

Institute for Defense Analyses Communications Research Division von Neumann Hall Princeton, New Jersey Commanding Officer
Office of Naval Research Branch
Office
495 Summer Street
Boston, Massachusetts 02110

Commanding Officer
Office of Naval Research Branch
Office
1000 Geary Street
San Francisco, California 94109

COR Arthur J. Coyle Office of Naval Research Code 429 Department of the Navy Washington, D.C. 20360

Mr. William C. Karl Office of Naval Research Code 429 Department of the Navy Washington, D.C. 20360

University of Chicago Statistical Research Center Chicago, Illinois 60637 Attn: Prof. Paul Meier

Stanford University
Department of Statistics
Stanford, California 94305
Attn: Prof. Gerald J. Lieberman

Florida State University Department of Statistics Tallahassee, Florida 32306 Attn: Dr. Ralph A. Bradley

Princeton University
Department of Mathematics
Princeton, New Jersey
Attn: Prof. J. Tukey

Columbia University
Department of Mathematical Statistics
New York 27, New York 10027
Attn: Prof. T.W. Anderson

Mr. Richard Hussey
Air Force Director of
Procurement Management
Room 4C253, Pentagon
Washington, D.C. 20301

Mr. B. Kurkjian Harry Diamond Laboratory Department of the Army Washington 25, D.C.

Mr. Seymour Lorber HQ, Army Material Command Department of the Army Washington 25, D.C.

Mr. Joseph Mandelson Directorate of Quality Assurance Edgewood Arsenal Edgewood, Maryland

Mr. Arthur Marthens Bureau of Ships Department of the Navy Room 3012, Main Navy Bldg. Washington, D.C. 20360

Major John F. Mosher Air Force System Command (SCSVE) Andrews Air Force Base Washington 25, D.C.

Dr. W.R. Pabst, Jr. Chief Statistician Bureau of Naval Weapons (P-130) Washington, D.C. 20360

Mr. T.M. Vining HQ, Defense Supply Agency Cameron Station Alexandria, Virginia

Mr. J. Weinstein Chief, Mathematics Division Institute for Experimental Research U.S. Army Electronics R and D Lab. Fort Monmouth, New Jersey

U.S. Naval Ordnance Test Station China Lake, California 93557 Attn: Statistics Branch (Code 5077)

Commanding Officer
U.S. Naval Underwater Ordnance Station
Newport, Rhode Island 02844
Attn: Library (Cm4b)

Commanding Officer U.S. Naval Torpedo Station Keyport, Washington Code 533 Code 334 (QEL Library)

Library Technical Reports Section U.S. Naval Postgraduate School Monterey, California 93940

Commander
Philadelphia Naval Shipyard
(Naval Boiler and Turbine Lab.)
Naval Base, Philadelphia, Pennsylvania
19112

Officer-in-Charge U.S. Naval Underwater Weapons Systems Engineering Center Newport, Rhode Island 02844 Attn: Quality Evaluation Lab. (QES)

Commanding Officer and Director U.S. Navy Electronics Lab. (Library) San Diego, California 92152

Commanding Officer and Director U.S. Navy Mine Defense Lab. Technical Library Panama City, Florida 32402

Commanding Officer and Director (Code 904)
U.S. Navy Underwater Sound Lab.
Fort Trumbull, New London, Conn. 06321

Commanding Officer
U.S. Naval Avionics Facility
Indianapolis, Indiana 46218
Attn: Library

Commanding Officer U.S. Naval Ammunition Depot (QETM) Crane, Indiana

Commanding Officer
U.S. Naval Ammunition Depot (QEL)
St. Juliens Creek
Portsmouth, Virginia 23702

Commanding Officer
U.S. Naval Weapons Station
Seal Beach, California 90740
Attn: Technical Library, Eldg. A0-2

Officer-in-Charge U.S. Naval Fleet Missile Systems Analysis and Evaluation Group Corona, California Mr. James C. Taylor (R-ASTR-R) Astrionics Laboratory NASA Marshall Space Flight Center Huntsville, Alabama 35812

Mr. J.E. Stitt (12.000) Instrument Research Division NASA Langley Research Center Langley Station Hamption, Virginia 23365

Mr. Roy E. Currie, Jr., (R-ASTR-TN) Astrionics Laboratory NASA Marshall Space Flight Center Huntsville, Alabama 35812

Mr. Fred L. Niemann
Assistant Director for Technical
Programs
NASA North Eastern Office
30 Memorial Drive
Cambridge, Massachusetts 02142

Mr. J. Brad Aaron NASA Wallops Station Wallops Island, Virginia 23337

Mr. Edward M. James, Jr., Chief Technical Division NASA Western Operations Office 150 Pico Boulevard Santa Monica, California 90406

Mr. Samuel Perrone, Assistant Chief Office of Reliability and Quality Assurance NASA Lewis Research Center 21000 Brookpark Road Cleveland, Ohio 44135

Mr. R. Body (PA-6) Chief, Apollo Reliability and Quality Assurance Office NASA J.F. Kennedy Space Center Cocoa Beach, Florida

Mr. George A. Lemke, Director Apollo Reliability and Quality Assurance Office (MAR) Office of Manned Space Flight NASA Headquarters Washington, D.C. 20546

Research Triangle Institute P.O. Box 490 Durham, North Carolina 27702 Attn: Project Officer NASr-40 Dr. Albert J. Kelley (RE-TG)
Office of Advanced Research
and Technology
NASA Headquarters
400 Maryland Avenue, S.W.
Washington, D.C. 20546

Mr. I.B. Altman
Office, Secretary of Defense (I and L)
Quality Control and Reliability
Room 1E815, Pentagon
Washington, D.C. 20301

Mr. Joseph Carroll Bureau of Naval Weapons Quality Evaluation Operations Code FQAO-3 Naval Weapons Plant Washington 25, D.C.

Mr. O.A. Cocca HQ, Air Force Logistics Command (MCPKQ) Wright-Patterson Air Force Base Ohio

Mr. James Coffin Air Force System Command (SCKAQ) Andrews Air Force Base Washington 25, D.C.

Mr. John Condon
Director, Office of Reliability
and Quality Assurance
NASA Headquarters, Code KR
Washington, D.C. 20546

Mr. Walter Foster Fort Detrick Frederick, Maryland

Mr. Fred Frishman OCRD, Department of the Army 419 3045 Columbia Pike Arlington, Virginia

Mr. Earl K. Yost Defense Supply Agency Cameron Station Alexandria, Virginia

Dr. Frank Grubbs Aberdeen Proving Grounds Aberdeen, Maryland

Mr. Silas Williams, Jr.

HQ, U.S. Army Supply and
Maintenance Command
Chief, Quality Assurance, AMSSM-QA
Washington, D.C. 20315

Yale University
Department of Statistics
New Haven, Connecticut 06520
Attn: Prof. L. J. Savage

Rocketdyne - A Division of North American Aviation, Inc. 6633 Canoga Avenue Canoga Park, California Attn: Dr. N. R. Goodman Dr. J. M. Zimmerman

Rutgers - The State University Statistics Center New Brunswick, New Jersey 08903 Attn: Prof. H.E. Dodge

Yale University
Department of Statistics
New Haven, Connecticut 06520
Attn: Prof. F.J. Anscombe

Purdue University Division of Mathematical Sciences Lafayette, Indiana 47907 Attn: Prof. S.S. Gupta

Cornell University
Department of Industrial Engineering
Ithaca, New York
Attn: Prof. Robert Bechhofer

Stanford University
Department of Statistics
Stanford, California 94305
Attn: Prof. C. Stein

Stanford University
Department of Statistics
Stanford, California 94305
Attn: Prof. H. Chernoff

Mr. John E. Condon
Director, Office of Reliability
and Quality Assurance, Code KR
NASA Headquarters
400 Maryland Avenue, S.W.
Washington, D.C. 20546

Mr. Dwight C. Cain (MGR)
Office of Manned Space Flight
Gemini Program Office
NASA Headquarters
400 Maryland Avenue, S.W.
Washington, D.C. 20546

Dr. John M. Walker (RET)
Office of Advanced Research
and Technology
NASA Headquarters
400 Maryland Ave., S.W.
Washington, D.C. 20546

Mr. James O. Spriggs (SA)
Office of Space Science and
Applications
NASA Headquarters
400 Maryland Avenue, S.W.
Washington, D.C. 20546

Mr. John V. Foster, Chief Systems Engineering Division NASA Ames Research Center Moffett Field, California 94035

Mr. Richard B. Cox, Head Quality Assurance Office NASA Flight Research Center P.O. Box 273 Edwards, California 93523

Mr. Clinton T. Johnson Reliability Analysis NASA Flight Research Center P.O. Box 273 Edwards, California 93523

Mr. G. Kambouris (232) Office of Technical Services NASA Goddard Space Flight Center Greenbelt, Maryland 20771

Dr. William Wolman (600)
Office of Space Science
and Satellite Applications
NASA Goddard Space Flight Center
Greenbelt, Maryland 20771

Mr. Brooks T. Morris, Chief Quality Assurance and Reliability Office Jet Propulsion Laboratory 4800 Oak Grove Drive Pasadena, California 91103

Mr. Eugene H. Britt
Reliability and Quality
Assurance Officer
NASA Langley Research Center
Langley Station
Hamption, Virginia 23365

Mr. T. J. Edwards (SR) NASA Manned Spacecraft Center 2101 Webster-Seabrook Road Houston, Texas 77058

Mr. Robert L. Chandler, (R-QUAL-R) NASA Marshall Space Flight Center Huntsville, Alabama 35812 University of California Department of Statistics Berkeley 4, California Attn: Prof. J. Neyman

University of Washington Department of Mathematics Seattle 5, Washington Attn: Prof. Z.W. Birnbaum

Cornell University
Department of Mathematics
Ithaca, New York
Attn: Prof. J. Wolfowitz

Harvard University Department of Statistics Cambridge, Massachusetts Attn: Prof. W.G. Cochran

Institute of Mathematical Statistics University of Copenhagen Copenhagen, Denmark Attn: Prof. Anders Hald

Columbia University
Department of Industrial Engineering
New York 27, New York 10027
Attn: Prof. Cyrus Derman

Columbia University
Department of Mathematics
New York 27, New York 10027
Attn: Prof. H. Robbins

New York University Institute of Mathematical Sciences New York 3, New York Attn: Prof. W. M. Hirsch

University of North Carolina Statistics Department Chapel Hill, North Carolina Attn: Prof. Walter L. Smith

Michigan State University Department of Statistics East Lansing, Michigan Attn: Prof. Herman Rubin

University of California, San Diego Department of Mathematics P.O. Box 109 La Jolla, California 92038 Attn: Prof. M. Rosenblatt New York University
Department of Industrial Engineering
and Operations Research
Bronx 63, New York
Attn: Prof. J. H. Kao

University of Wisconsin Department of Statistics Madison, Wisconsin Attn: Prof. G. E. P. Box

The Research Triangle Institute Statistics Research Division 505 West Chapel Hill Street Durham, North Carolina Attn: Dr. Malcolm R. Leadbetter

Florida State University Department of Statistics Tallahassee, Forida 32306 Attn: Prof. I.R. Savage

Massachusetts Institute of Technology Department of Electrical Engineering Cambridge, Massachusetts 02139 Attn: Dr. R.A. Howard

The Johns Hopkins University
Department of Mathematical Statistics
34th and Charles Streets
Baltimore 18, Maryland
Attn: Prof. Geoffrey S. Watson

Stanford University
Department of Statistics
Stanford, California 94305
Attn: Prof. E. Parzen

Arcon Corporation 803 Massachusetts Avenue Lexington 73, Massachusetts 02173 Attn: Dr. Arthur Albert

University of California College of Engineering Operations Research Center Berkeley, California Attn: Prof. R.E. Barlow

Michigan State University Department of Statistics East Lansing, Michigan Attn: Prof. J. Gani U.S. Naval Fleet Missile Systems Analysis and Evaluation Group Corona, California 91720

Commander
U.S. Naval Ordance Laboratory
White Oak
Sivler Spring, Maryland
Code (MS Div)
Code (R - Dept)

Commanding Officer U.S. Naval Weapons Station (QEW) Concord, California

Officer-in-Charge U.S. Naval Mine Engineering Facility U.S. Naval Weapons Station Yorktown, Virginia - 23491

Commanding Officer
U.S. Naval Propellant Plant
Indian Head, Maryland
Code (QA)
Code (REM)

Commander
U.S. Naval Weapons Laboratory
Dahlgren, Virginia
Attn: Technical Library

Chief, Bureau of Naval Weapons
Department of the Navy
Washington, D.C. 20360
Code (FQ)
Code (PQC)
Code (P-13)
Code (RAAV-33)

Chief of Naval Material (MAT-254) Department of the Navy Room 3025, Munitions Bldg. Washington, D.C. 20360

Director
U.S. Naval Weapons Quality Assurance Office
Quality Analysis Department
Washington Navy Yard
Washington, D.C. 20390

Chief of Naval Operations (Op-03EG) Operations Evaluation Group The Pentagon Washington, D.C. 20350

Commanding Officer (ADLR)
U.S. Naval Air Development Center
Johnsville, Pa.
Attn: NADC Library

Commander
U.S. Naval Missile Center
Point Mugu, California

Attn: Technical Library, Code No 322

Commanding Officer
U.S. Naval Construction Battalion
Center
Gulfport, Mississippi

U.S. Naval Construction Battalion Center Port Hueneme, California 93041 Code 92

U.S. Naval Ammunition Depot Navy No. 66, c/o FPO San Francisco, California 96612 Attn: Weapons Technical Library

Commander, U.S. N.O.T.S. Pasadena Annex 3202 East Foothill Blvd. Pasadena, California 91107 Attn: Pasadena Annex Library